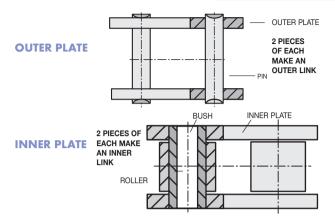
CHAIN INFORMATION

Technical Section



CHAIN STANDARDS			
AMERICAN ANSI B29.1 : ISO 606 A SERIES			
BRITISH	BS 228 : DIN 8187 : ISO 606		

Lubrication (Dependent on power and speed)

TYPE 1 : MANUAL TYPE 2 : DRIP FEED TYPE 3 : OIL BATH TYPE 4 : OIL STREAM

See Chart on page 27.65.

RECOMMENDED LUBRICANTS AMBIENT TEMPERATURE					
°C	°F (Approx.)	LUBRICANT RAT			
		SAE	BS4231		
-5 to 5	20 to 40	20	46 - 68		
5 to 40	40 to 100	30	100		
40 to50	100 to 120	40	150 - 220		
50 to 60 120 to 140 50 320					

BREAKING STRENGTHS

PART NUMBER	PITCH		Weight Kg/m		
Steel					
SUA-4	4.00	1800	0.07		
SUA-6	6.00	3000	0.12		
SUA-250	6.35	4000	0.13		
SBR-8	8.00	5000	0.18		
SUA-375	9.53	10000	0.33		
SBR-375	9.53	11100	0.39		
SUA-500	12.70	16900	0.63		
SBR-500	12.70	19000	0.70		
SUA-541	12.70	10600	0.42		
SBR-625	15.89	23000	0.92		
SUA-750	19.05	30500	1.20		
SBR-1000	25.40	67000	2.80		
SBR-1250	31.75	98070	3.85		

Stainless Steel

SBS-6	6.00	2000	0.12
SBS-8	8.00	4000	0.18
SUS-375	9.53	7560	0.33
SBS-375	9.53	7000	0.41
SUS-500	12.70	10690	0.63
SBS-500	12.70	11770	0.68
SBS-625	15.875	14700	0.92





CHAIN SELECTION PROCESS Technical Section

STEP (1)

SELECT DRIVE RATIO AND SPROCKETS

Chart 1 may be used to choose a ratio based on the standard sprocket sizes available. It is best to use an odd number of teeth combined with an even number of chain pitches.

Ideally, chain sprockets with a minimum of 19 teeth should be chosen. If the chain drive operates at high speed or is subjected to impulsive loads, the smaller sprockets should have at least 25 teeth and should be hardened.

It is recommended that chain sprockets should have a maximum of 114 teeth.

Drive ratio can otherwise be calculated using the formula:-

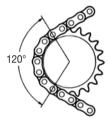
$$i = \frac{Z_2}{Z_1}$$

For large ratio drives, check that the angle of lap on Z1 is not less than 120°.

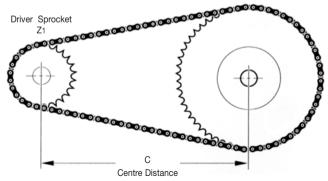
NO. OF TEETH DRIVEN SPROCKET Z2	NO. OF TEETH DRIVE SPROCKET Z1					
	15	17	19	21	23	25
25	-	-	-	-	-	1.00
38	2.53	2.23	2.0	1.80	1.65	1.52
57	3.80	3.35	3.0	2.71	2.48	2.28
76	5.07	4.47	4.0	3.62	3.30	3.04
95	6.33	5.59	5.0	4.52	4.13	3.80
114	7.60	6.71	6.0	5.43	4.96	4.56

Chart 1

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CHAIN SELECTION PROCESS

Technical Section

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STEP (2)

APPLICATION FACTOR f1

Factor f1 takes account of any dynamic overloads depending on the chain operating conditions., The value of factor f1 can be chosen directly or by analogy using Chart 2.

TOOTH FACTOR f2

The use of a tooth factor further modifies the final power selection. The choice of a smaller diameter sprocket will reduce the maximum power capable of being transmitted since the load in the chain will be higher.

$$f2 = \frac{19}{Z_1}$$

Note that this formula arises due to the fact that selection rating curves shown in the BS/ANSI rating charts are those foa a 19 tooth sprocket.

f2 factors	for	standard	sprocket	sizes.
------------	-----	----------	----------	--------

Z1	f2
15	1.27
17	1.12
19	1.00
21	0.91
23	0.83
25	0.76

Chart 2

	CHARACTERISTICS OF DRIVER			
DRIVEN MACHINE CHARACTERISTICS	SMOOTH RUNNING electric motors, Steam and gas turbines, internal combustion, engines with hydraulic coupling		MODERATE SHOCKS internal combustion engines with less than 6 cyls, with mechanical coupling	
SMOOTH RUNNING centrifugal pumps and compressors, printing machines, paper calenders, uniformly loaded conveyors, escalators, liquid agitators and mixers, rotary driers, fans	1	1.1	1.3	
MODERATE SHOCKS pumps and compressors (3+ cyls), concrete mixing machines, non uniformly loaded conveyors, solid agitators and mixers.	1.4	1.5	1.7	
HEAVY SHOCKS planers, excavators, roll and ball mills, rubber processing machines, presees and shears, 1 & 2 cyl pumps and compressors, oil drilling rigs	1.8	1.9	2.1	

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CHAIN SELECTION PROCESS Technical Section

STEP ③

CALCULATE THE SELECTION POWER

Multiply the power to be transmitted by the factors obtained from STEP TWO.

Selection POWER = POWER to be transmitted x f1 x f2 (kw). This selection power can be used with the appropriate rating chart on page 27.65.

STEP 4 SELECT CHAIN DRIVE

From the rating chart, select the smallest pitch of sample chain to transmit the SELECTION POWER at the speed of the driving sprocket Z1.

This normally results in the most economical drive selection. If the SELECTION POWER is now greater than that shown for the simple chain, then consider a multiplex chain of the same pitch size as detailed in the rating charts.

STEP (5)

To find the chain length pitches (L) for any contemplated centre distance of a two point drive, use the formula below:-

Length (L) =
$$\frac{Z_1 + Z_2}{2} + \frac{2C}{P} + \frac{\left(\frac{Z_2 - Z_1}{2\pi}\right)^2 x P}{C}$$

The calculated number of pitches should be rounded up to a whole number of even pitches. Odd numbers of pitchers should be avoided because this would involve the use of a cranked link which is not recommended. If a jockey socket is used for adjustment purposes, two pitches should be added to the chain length [L).

C is the contemplated centre distance in mm and should generally be between 30 - 50 pitches.

STEP 6 CALCULATE EXACT CENTRE DISTANCE

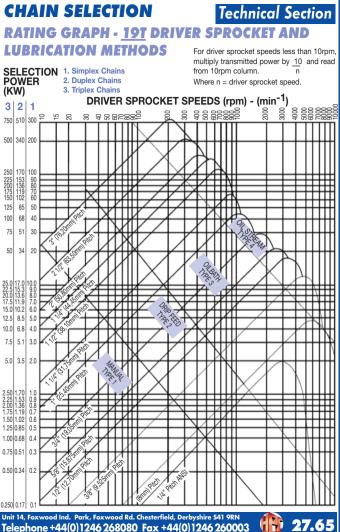
The actual centre distance for the chain length (L) calculated by the method above, will in general be greater than that originally contemplated. The revised centre distance can be calculated from the formula below.

$$C = \frac{P}{8} \left[2L - Z2 - Z1 + \sqrt{(2L - Z_2 - Z_1)^2 - \left(\frac{\pi}{3.88} - (Z_2 - Z_1)^2\right)} \right]$$

P = Chain pitch (mm) L = Chain length (pitches) Z₁= Number of teeth in driver sprocket

 Z_{2} = Number of teeth in driven sprocket Z_{2} = Number of teeth in driven sprocket





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CHAIN CONNECTING LINKS SIMPLEX, DUPLEX & TRIPLEX







These links should not be used where high speed or arduous conditions apply, in these cases, where safety is essential, a riveting link (interference fit) must be used. NOTE: Some dimensions on Pin Length may differ slightly.

Triplex

			D: 0		
PART NUMBER	Chain No.	Pitch (mm)	Pin Ø (mm)	Pin Length (mm)	Con Link Extra (mm)
	onum rec.	()	()	Longer (min)	Exact (min)
Stainless Steel					
SBS-6/L	04-SS	6	1.85	7.4	2.9
SBS-8/L	08B-SS	8	2.31	9.0	-
SUS-375/L	35-SS	9.525	3.59	15.15	3.3
SBS-375/L	06B-SS	9.525	3.28	14.0	-
SUS-500/L	40-SS	12.70	3.98	17.8	3.9
SBS-500/L	08B-SS	12.70	4.45	17.5	3.9
SBS-625/L	10B-SS	15.875	5.08	20.0	4.1
Simplex					
SUA-4/L	1141	4	1.65	6.8	1.2
SUA-6/L	04	6	1.85	7.4	2.9
SUA-250/L	25	6.35	2.30	8.6	0.8
SBR-8/L	05B-1	8	2.31	8.6	3.1
SUA-375/L	35	9.525	3.59	15.5	3.3
SBR-375/L	06B-1	9.525	3.28	13.5	3.3
SUA-500/L	40	12.7	3.98	17.8	3.9
SBR-500/L	08B-1	12.7	4.45	17.0	3.9
SUA-541/L	41	12.7	3.59	14.5	2.0
SBR-625/L	10B-1	15.875	5.08	18.8	4.1
SUA-750/L	12B-1	19.05	5.72	22.7	4.6
SBR-1000/L	16B-1	25.40	8.28	36.1	5.4
SBR-1250/L	20B-1	31.75	10.19	43.2	6.1
Duplex					
XSBR-8/L	05B-2	8.00	2.31	14.3	3.1
XSBR-375/L	06B-2	9.52	3.28	23.8	3.3
XSBR-500/L	08B-2	12.70	4.45	31.0	3.9
XSBR-625/L	10B-2	15.875	5.08	35.4	4.1
XSUA-750/L	12B-2	19.05	5.72	42.2	4.6
Triplex					
XXSBR-375/L	06B-3	9.52	3.28	34.0	3.3
XXSBR-500/L	08B-3	12.70	4.45	44.9	3.9
XXSBR-625/L	10B-3	15.875	5.08	52.8	4.1
XXSUA-750/L	12B-3	19.05	5.72	61.7	4.6
			, Foxwood Rd. Cl		-



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HOSTAFORM C

Technical Section

HOSTAFORM C 9021 K ACETAL COPOLYMER WITH

SPECIAL CHALK

Physical Properties	Metric
Density	1.44 g/cc
Water Absorption	0.2%
Water Absorption at Saturation	0.65%
Melt Flow	10.8 g/10 min
Mechanical Properties	
Ball indentation Hardness	145 MPa
Tensile Strength, Yield	60 MPa
Elongation at Break	22%
Elongation at Yield	8%
Tensile Modulus	3 GPa
Flexural Modulus	2.9 GPa
Charpy Impact Unnotched	10 J/cm ²
Charpy Impact Notched, Low Temp	0.5 J/cm ²
Charpy Impact Unnotched, Low Temp	10 J/cm ²
Charpy Impact, Notched	0.6 J/cm ²
Tensile Creep Modulus, 1 hour	2500 MPa
Tensile Creep Modulus, 1000 hour	1400 MPa
Electrical Properties	
Dielectric Constant	4.2
Dielectric Constant, Low Frequency	4.2
Dielectric Strength	38 kV/mm
Dissipation Factor	0.006
Dissipation Factor, Low Frequency	0.0025
Thermal Properties	
CTE, Linear 20 C	110 µm/m-°C
Melting Point	166 °C
Deflection Temperature at 1.8 MPa (264 psi)	100 °C
Vicat Softening Point	150 °C

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